

grid. It has been controlled by STATCOM using Fuzzy Logic Controller (FLC). The FLC is tuned offline, by a fuzzy model and a set of fuzzy rules as shown in Table I.

TABLE I. FUZZY RULES

Rule No.	Fuzzy Input		Fuzzy Output	
	Tf_1	Tf_2	Q_{RSC}	$Q_{STATCOM}$
1.	IF HIGH	HIGH	THEN MEDIUM	HIGH
2.	IF HIGH	MEDIUM	THEN MEDIUM	HIGH
3.	IF HIGH	LOW	THEN HIGH	HIGH
4.	IF MEDIUM	HIGH	THEN LOW	HIGH
5.	IF MEDIUM	LOW	THEN HIGH	HIGH
6.	IF LOW	HIGH	THEN LOW	LOW
7.	IF LOW	MEDIUM	THEN LOW	LOW

B. The Reactive Power Control Technique

Fig. 2 shows that, there are two states for switches S_1 and S_2 . During normal condition, the switches S_1 and S_2 are closed in state 1. In this state the initial reactive power limits, denoted as Q_{RSC}^0 and $Q_{STATCOM}^0$ are maintained. During fault condition, the switches are transferred to state 2. The Fuzzy Logic Controller (FLC) acts suddenly and provides the optimal control values namely Q_{RSC}^* and $Q_{STATCOM}^*$ to control the STATCOM which in turn compensates the required reactive power in order to maintain the transient stability. The two sensitivity indices namely Voltage Severity Index (VSI) and Transient Power Severity Index (TPSI) are necessary to optimize the control parameters, through which Var compensation is achieved. The operation of FLC is based on fuzzy rules as shown in Table. I. The fuzzy subsets for the input variables, Tf_1 and Tf_2 is shown in Fig. 3. The fuzzy subsets for the output variables Q_{RSC}^* and $Q_{STATCOM}^*$ are shown in Fig. 4 and Fig. 5 respectively. Table II and III shows the initiating values of parameters, m and σ , for the input and output fuzzy subsets.

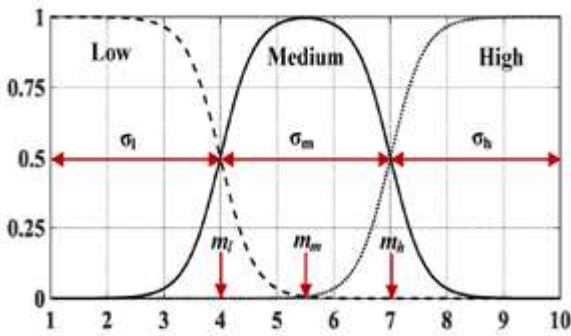


Fig. 3. Fuzzy input subsets of Tf_1 and Tf_2

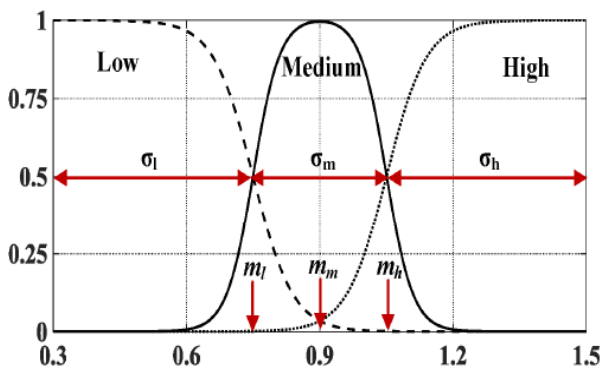


Fig. 4. Fuzzy output subsets of Q_{RSC}^*

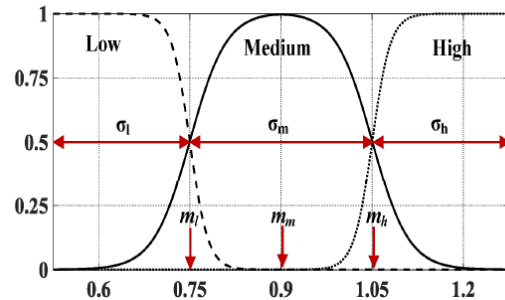


Fig. 5. Fuzzy output subsets of $Q_{STATCOM}^*$

TABLE II. PARAMETERS TO INITIATE SIGMOIDAL MEMBERSHIP FOR INPUT, OUTPUT VARIABLES

Variable s	Variables range	Low	Subset	Medium	Subset	High	Subset
		m_l	σ_l	m_m	σ_m	m_h	σ_h
$Tf_{1,2,3}$	[1, 2, ...10]	4	3	5.5	3	7	3
Q_{RSC}^*	(0.3 1.5)	0.75	0.45	0.9	0.3	1.05	0.45
$Q_{STATCOM}^*$	(0.5 1.275)	0.75	0.225	0.9	0.3	1.05	0.225

TABLE III. PARAMETERS TO INITIATE SIGMOIDAL MEMBERSHIP FOR OUTPUT VARIABLES

Variables	Low	Subset	Medium	Subset	High	Subset
	m_l	σ_l	m_m	σ_m	m_h	σ_h
Q_{RSC}^*	y_1	0.45	$y_1+0.15$	0.3	$y_1+0.3$	0.45
$Q_{STATCOM}^*$	y_2	0.225	$y_2+0.15$	0.3	$y_2+0.3$	0.225

III. PROBLEM FORMULATION

A. Objective function

The objective function is to minimize Voltage Severity Index (VSI) and Transient Power Severity Index (TPSI) given by equation 1 to 3. The objective function is subjected to both linear and non-linear constraints which are discussed in detail in the next section

$$VSI = \frac{\sum_{t=T_s}^T \Delta V_{PCC}^t}{T - T_s} \tag{1}$$

$$\Delta V_{PCC}^t = \begin{cases} \frac{V_{PCC}^t - V_{PCC}^0}{V_{PCC}^0} & \text{if } \frac{V_{PCC}^t - V_{PCC}^0}{V_{PCC}^0} \geq \alpha \\ 0 & \text{otherwise} \end{cases} \tag{2}$$

$$TPSI = \frac{\sum_{i=1}^N \sum_{t=T_c}^T \left(\frac{|P_i^t - P_i^0|}{P_i^0} \right)}{N * (T - T_c)} \tag{3}$$

where

V_{PCC}^0 - Voltage at PCC at time, $T=0$

V_{PCC}^t - Voltage at PCC at time, $T=t$

α - Voltage change outside the specified

limits ($\pm 5\%$)

N - Number of buses

T_c - Fault clearing time

P_i^0 - Real power during pre-fault condition

P_i^t - Real power at time, $T=t$

B. Constraints

The linear constraints are the real and reactive power balance given by equations 4 and 5.

$$P_G - P_L - P(V, \theta) = 0 \quad (4)$$

$$Q_G - Q_L - Q(V, \theta) = 0 \quad (5)$$

The non-linear constraints are denoted by set of equations in 6, which includes, apparent power limit (S), Voltage limit at various buses (V, $\angle\theta$), limits of real and reactive power of generators, reactive power limits of STATCOM

$$\left. \begin{aligned} S(V, \theta) &\leq S_{\max} \\ V_{\min} &\leq V \leq V_{\max} \\ P_G^{\min} &\leq P_G \leq P_G^{\max} \quad Q_G^{\min} \leq Q_G \leq Q_G^{\max} \\ Q_{STAT}^{\min} &\leq Q_{STAT} \leq Q_{STAT}^{\max} \end{aligned} \right\} \quad (6)$$

The non-linear constraints also consists of change in rotor angle $\Delta\delta$ at time $t=T$ should be within the tolerance limit β as given by equation 7.

$$[\max(\Delta\delta_{ij}^T)] \leq \beta \quad (7)$$

By using the fuzzy logic controller, the control variables (QRSC and QSTATCOM) are adjusted with the help of the two parameters namely y_1 and y_2

$$\left. \begin{aligned} 0.3 &\leq Q_{RSC} \leq 2MVar \\ 0.5 &\leq Q_{STAT} \leq 2MVar \\ 0.7 &\leq y_1 \leq 0.8, 0.7 \leq y_2 \leq 0.8 \end{aligned} \right\} \text{ is shown in equation } \alpha \quad (8)$$

To begin with the solutions for the control variables represented by, $X = [Q_{RSC}, Q_{STATCOM}]$ and adjusting parameters of FLC, denoted as, $Y = [y_1, y_2]$ are initiated using equation 9 to 11 respectively.

$$X_{new} = X_{iter} + (X_{\max} - X_{iter}) \cdot \text{rand}(0,1) \cdot \exp(-iter / \max iter) \quad (9)$$

$$X_{new} = X_{iter} + (X_{iter} - X_{\min}) \cdot \text{rand}(0,1) \cdot \exp(-iter / \max iter) \quad (10)$$

$$Y_{new} = Y_{iter} + \text{rand}(-0.5, 0.5) \cdot \left[\frac{Tf_1^{iter} + Tf_2^{iter}}{Tf_1^{initial} + Tf_2^{initial}} \right] \quad (11)$$

The change in control variables are denoted as Δf_1 and Δf_2 are shown in equations 12 and 13 respectively which contributes for the final objective functions

$$\Delta f_1 = f_1^{norm}(Q_{RSC}^{new}, Q_{STAT}^{new}) - f_1^{norm}(Q_{RSC}^{iter}, Q_{STAT}^{iter}) \quad (12)$$

$$\Delta f_2 = f_2^{norm}(Q_{RSC}^{new}, Q_{STAT}^{new}) - f_2^{norm}(Q_{RSC}^{iter}, Q_{STAT}^{iter}) \quad (13)$$

IV. THE CASE STUDY USED FOR SIMULATION

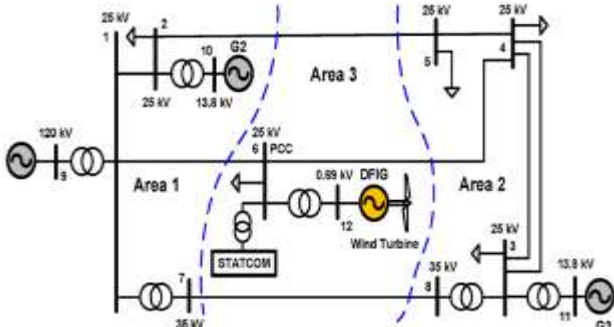


Fig. 6. Fuzzy based STATCOM controller for a 12 bus power system [15].

The power system considered for the study consists of 12 buses and 4 generators. The same simulated using MATLAB_SIMULINK with a wind turbine and a STATCOM controller, located at the Point of Common Coupling which is at bus 6 is shown in Fig. 6. The system is divided into three areas. The first area consists of generators G1 as well as G2. Generator G3 is in the load side which forms the second area. Doubly-Fed Induction Generator (DFIG) based wind turbine which under consideration for the study proposed, is rated at 2 MW and a 2 MVar STATCOM, are associated with the third area. The speed of the rotor is 1.2 p.u. A transformer, rated at 0.69/25 kV is used to connect the DFIG to the grid. A three phase PWM converter is used to supply the rotor. A transformer rated at 13.8/25 kV is used to connect the STATCOM at the bus 6 which is the Point of Common Coupling. The system is simulated for the most sever symmetrical type of fault namely the three phase fault between bus 1 and bus 6. The time of fault simulation is enoted as, $T_s = 50$ s and the time of fault clearing is represented as, $T_c = 200$ ms.

V. RESULTS AND DISCUSSION

The graphical results of a 12 bus power system consist of a DFIG based wind turbine, equipped with a fuzzy logic based STATCOM controller, simulated with a three phase symmetrical fault are shown in Fig. 7 to Fig. 10. The rate of change of voltage magnitude at the point of common coupling during the fault is shown in Fig. 7. The transient voltage stability of the power system is optimally maintained, after clearing the fault through reactive power compensation offered by the STATCOM. It is clearly depicted in Fig. 8 that the low frequency real power oscillations are mitigated by the intelligent behavior of FLC based STATCOM controller during post fault conditions. The variations of control variables namely $Q_{STATCOM}$, and Q_{RSC} , with respect to time are during pre-fault and post-fault simulations are shown in Fig. 9 and Fig. 10 respectively.

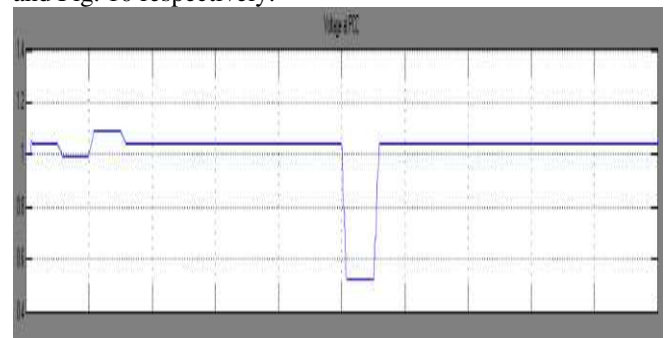


Fig. 7. MATLAB_SIMULINK output for voltage at PCC during 3 phase fault

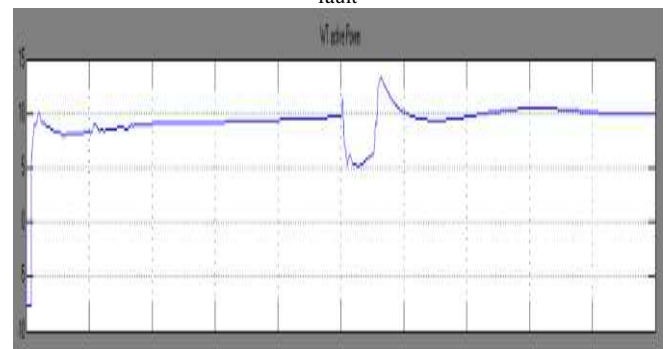


Fig. 8. Active power oscillations at the wind turbine during three phase fault

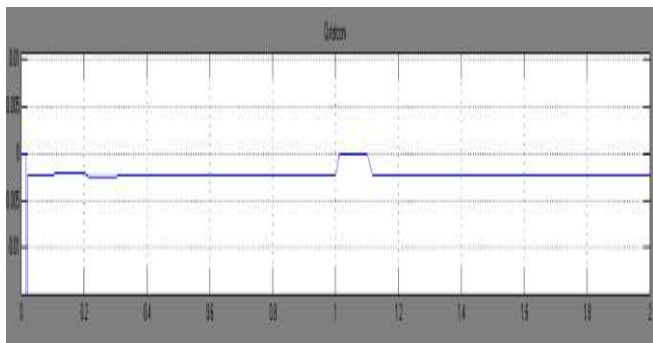


Fig. 9. MATLAB_SIMULINK output for $Q_{STATCOM}$ during three phase fault



Fig. 10. MATLAB_SIMULINK output for Q_{RSC} during three phase fault

VI. CONCLUSION

This work presents a VAR compensation strategy of DFIG based wind turbine using STATCOM. A multi-objective problem will be formulated to improve the voltage stability by maintaining within its rated limits using VSI and to mitigate low frequency oscillations by using TPSI during three phase fault conditions. The solution for the proposed problem is optimized using Fuzzy Logic. In order to justify the proposed methodology it is modeled in a 12 bus power system [15] with a 2 MW DFIG using MATLAB- Simulink. The system is then tested by simulating a three phase fault. The graphical results of the case study are analyzed and presented. It is inferred from the results, that the fuzzy based reactive controller is effective in optimizing the power flow even during fault conditions.

In future, this work can be extended by using other types of FACTS controllers like SVC, TCSC, etc. The same work will also be implemented for higher bus power systems like IEEE 30, 57, 118, 300 buses. The same problem can also be studied by simulating various unsymmetrical faults, like, single line to ground (LG), double line to ground (LLG) and double line (LL) faults.

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